## Appendix 5

Calculations supporting the selection of $5 \times 150 \mathrm{~mm}$ diameter novacoil pipe that Releases clearwater from the coffer dam at the bottom of the link access track into the Papawai Stream

Catchment Area: 3000m²
HIRDs V4 Output:

Output Table Format

- Depth - Duration - Frequency
O Intensity - Duration - Frequency Generate Report

| ARI | AEP | 10 m | 20 m | 30 m | 1 h | 2 h | 6 ' | 12h | 24h | 48h | 72h | 96h | 120h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.58 | 0.633 | 6.94 | 9.85 | 12.0 | 16.8 | 23.0 | 36.8 | 48.2 | 61.7 | 76.9 | 86.4 | 93.3 | 98.6 |
| 2 | 0.500 | 7.63 | 10.8 | 13.2 | 18.4 | 25.2 | 40.2 | 52.6 | 67.3 | 83.9 | 94.2 | 102 | 107 |
| 5 | 0.200 | 10.0 | 14.1 | 17.2 | 23.9 | 32.8 | 52.1 | 68.0 | 86.6 | 108 | 121 | 130 | 137 |
| 10 | 0.100 | 11.8 | 16.7 | 20.3 | 28.2 | 38.5 | 61.0 | 79.4 | 101 | 125 | 140 | 151 | 160 |
| 20 | 0.050 | 13.7 | 19.3 | 23.5 | 32.5 | 44.4 | 70.2 | 91.2 | 116 | 144 | 161 | 173 | 182 |
| 30 | 0.033 | 14.9 | 20.9 | 25.5 | 35.2 | 48.0 | 75.7 | 98.4 | 125 | 155 | 173 | 186 | 196 |
| 40 | 0.025 | 15.7 | 22.1 | 26.9 | 37.2 | 50.6 | 79.8 | 104 | 131 | 162 | 182 | 195 | 206 |
| 50 | 0.020 | 16.4 | 23.1 | 28.0 | 38.7 | 52.7 | 82.9 | 108 | 136 | 169 | 188 | 203 | 214 |
| 60 | 0.017 | 17.0 | 23.8 | 28.9 | 40.0 | 54.4 | 85.6 | 111 | 141 | 174 | 194 | 209 | 220 |
| 80 | 0.012 | 17.8 | 25.1 | 30.4 | 42.0 | 57.1 | 89.7 | 116 | 147 | 182 | 203 | 218 | 230 |
| 100 | 0.010 | 18.5 | 26.0 | 31.6 | 43.6 | 59.2 | 93.0 | 120 | 152 | 188 | 210 | 226 | 238 |
| 250 | 0.004 | 21.5 | 30.1 | 36.5 | 50.2 | 68.1 | 107 | 138 | 174 | 214 | 239 | 257 | 270 |

The 100yr ARI (AEP 0.01) for 10 mins is $18.5 \mathrm{~mm} .3000 \mathrm{~m}^{2} \times 0.018 \mathrm{~m}=54 \mathrm{~m}^{3}$
$54 \mathrm{~m}^{3} / 10$ minutes is the same as 90 Litres per second assuming all rainfall immediately runs off and is distributed over the 10-minute period evenly.

The capacity of a 150 mm diameter pipe has been calculated as $21 \mathrm{~L} / \mathrm{s}$ using Manning's equation, an assuming the slope is $1 \%$ on the pipe and Manning's " n " is 0.013

$$
\begin{aligned}
Q & =A * V \\
V & =\frac{1}{n} * A^{*} \mathrm{R}^{2 / 3 *} \sqrt{S} \\
R & =\mathrm{A} / \mathrm{P}
\end{aligned}
$$

Conclusion: The combined flow capacity of the proposed $5 \times 150 \mathrm{~mm}$ diameter novacoil pipes ( $105 \mathrm{~L} / \mathrm{s}$ ) will accommodate $100 \%$ of the flow generated by the 100 yr ARI for the 10 minute event (90L/s). The assumptions made regarding how the flow is generated (namely zero infiltration and making no allowances for water travelling from distance) are unrealistic and conservative in nature and actual flows are likely to be considerably less.

