## Appendix 5

Calculations supporting the selection of a 300mm diameter pipe that "feeds" SRP1 (Lower Playing Field SRP). Catchment Area: 5000m²

HIRDs V4 Output:

7) 11
Output Table Format

- Depth - Duration - Frequency
O Intensity - Duration - Frequency Generate Report

| ARI | AEP | 10 m | 20m | 30 m | 1h | 2 h | 6 ' | 12h | 24h | 48h | 72h | 96h | 120h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.58 | 0.633 | 6.94 | 9.85 | 12.0 | 16.8 | 23.0 | 36.8 | 48.2 | 61.7 | 76.9 | 86.4 | 93.3 | 98.6 |
| 2 | 0.500 | 7.63 | 10.8 | 13.2 | 18.4 | 25.2 | 40.2 | 52.6 | 67.3 | 83.9 | 94.2 | 102 | 107 |
| 5 | 0.200 | 10.0 | 14.1 | 17.2 | 23.9 | 32.8 | 52.1 | 68.0 | 86.6 | 108 | 121 | 130 | 137 |
| 10 | 0.100 | 11.8 | 16.7 | 20.3 | 28.2 | 38.5 | 61.0 | 79.4 | 101 | 125 | 140 | 151 | 160 |
| 20 | 0.050 | 13.7 | 19.3 | 23.5 | 32.5 | 44.4 | 70.2 | 91.2 | 116 | 144 | 161 | 173 | 182 |
| 30 | 0.033 | 14.9 | 20.9 | 25.5 | 35.2 | 48.0 | 75.7 | 98.4 | 125 | 155 | 173 | 186 | 196 |
| 40 | 0.025 | 15.7 | 22.1 | 26.9 | 37.2 | 50.6 | 79.8 | 104 | 131 | 162 | 182 | 195 | 206 |
| 50 | 0.020 | 16.4 | 23.1 | 28.0 | 38.7 | 52.7 | 82.9 | 108 | 136 | 169 | 188 | 203 | 214 |
| 60 | 0.017 | 17.0 | 23.8 | 28.9 | 40.0 | 54.4 | 85.6 | 111 | 141 | 174 | 194 | 209 | 220 |
| 80 | 0.012 | 17.8 | 25.1 | 30.4 | 42.0 | 57.1 | 89.7 | 116 | 147 | 182 | 203 | 218 | 230 |
| 100 | 0.010 | 18.5 | 26.0 | 31.6 | 43.6 | 59.2 | 93.0 | 120 | 152 | 188 | 210 | 226 | 238 |
| 250 | 0.004 | 21.5 | 30.1 | 36.5 | 50.2 | 68.1 | 107 | 138 | 174 | 214 | 239 | 257 | 270 |

The 100 yr ARI (AEP 0.01) for 10 mins is $18.5 \mathrm{~mm} .5000 \mathrm{~m}^{2} \times 0.018 \mathrm{~m}=92.5 \mathrm{~m}^{3}$
$92.5 \mathrm{~m}^{3} / 10$ minutes is the same as 154 Litres per second assuming all rainfall immediately runs off and is distributed over the 10-minute period evenly.

The capacity of the 300mm diameter pipe has been calculated as $135 \mathrm{~L} / \mathrm{s}$ using Manning's equation, an assuming the slope is $1 \%$ on the pipe and Manning's " $n$ " is 0.013
$Q=A * V$
$V=\frac{1}{n} * \mathrm{~A}^{*} \mathrm{R}^{2 / 3 *} \sqrt{S}$
$R=\mathrm{A} / \mathrm{p}$

Conclusion: The flow capacity of the proposed 300 mm diameter pipe ( $135 \mathrm{~L} / \mathrm{s}$ ) will accommodate approximately $88 \%$ of the flow generated by the 100 yr ARI for the 10 minute event ( $154 \mathrm{~L} / \mathrm{s}$ ). The assumptions made regarding how the flow is generated (namely zero infiltration and making no allowances for water travelling from distance) are unrealistic and conservative in nature and actual flows are likely to be considerably less.

Despite the pipe capacity being theoretical short of $20 \mathrm{~L} /$ s over the minutes, the water that couldn't get through the pipe would back up behind the 550 mm bunds and make its way through the pipe as the water levels behind the bund subsided.

